

**US Army Corps
of Engineers®**
Engineer Research and
Development Center

Benefits of Inclusion of Geosynthetic Products in Reinforcement of Flexible Airfield Pavements Using Three- Dimensional Finite Element Modeling

**Cesar Tirado, Cesar Carrasco,
Gregory J. Norwood, Soheil Nazarian
and Jeb S. Tingle**



Objectives

- Determine benefits provided by geosynthetic reinforcement to flexible pavements
- 3D finite element model
 - Membrane and interface elements used for modeling geosynthetic material and its geomaterial interaction
- Evaluate most relevant properties

Traffic Benefit Ratio

- Assess effectiveness of a geosynthetic material in extending pavement service life
 - Defined as the ratio of the number of load cycles on a reinforced section to reach a defined failure state to the number of load cycles on an unreinforced section, with the same geometry and material constituents, to reach the same defined failure state

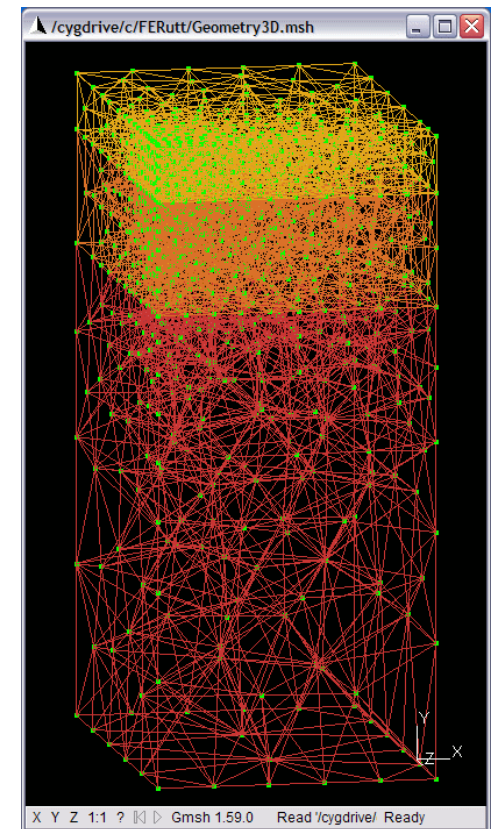
$$TBR = \frac{N_{\text{geogrid reinforced}}}{N_{\text{unreinforced}}}$$

Finite element model

- Use of available FEA software
 - 3-D FE code, suitable for flexible pavement analysis
 - Linear or nonlinear analysis
 - Nonlinear
 - Based on a modified linear elastic behavior
 - Endorses a universal relationship for both fine and coarse grained base and subgrade material (Uzan, 1985)

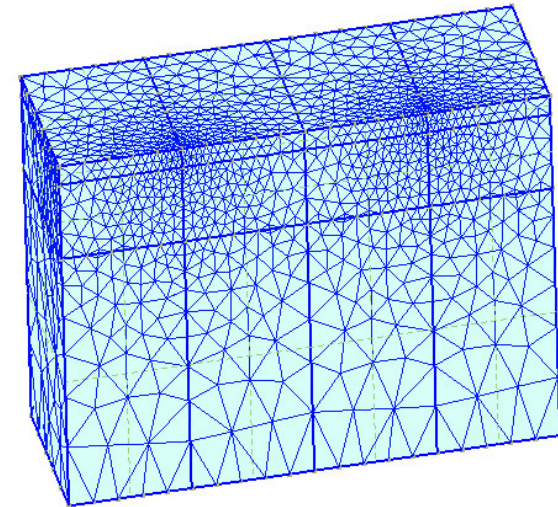
$$E = k_1 \sigma_c^{k_2} \sigma_d^{k_3}$$

- E : resilient modulus
- σ_c : confining pressure
- σ_d : deviatoric stress
- k_1, k_2, k_3 : coefficients statistically determined from results of laboratory resilient modulus tests.



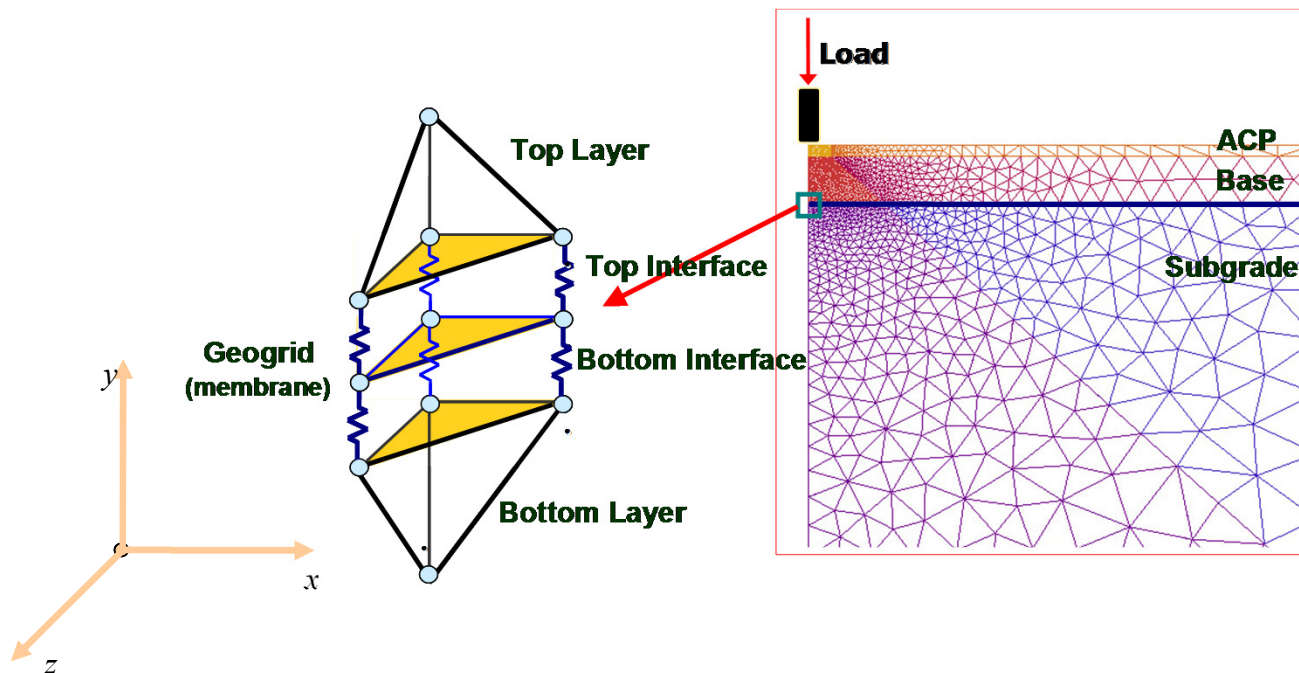
3-D Finite Element Model

- Simulate both reinforced and unreinforced pavement sections
 - Mesh generated based on axle configuration
 - Four-node tetrahedral elements mesh
- Justification for using 3D analysis to model the pavement system
 - It better reflects the complex behavior of the composite pavement system materials
 - Preferred for the verification of the numerical model results with laboratory or field test
 - Capable of simulating the rectangular footprint of the loaded wheel



Geosynthetic Materials

- Geomembrane modeled by a three-noded triangular membrane element
- Geogrid membrane element consist of three nodes
- Interface elements used for soil-geogrid interaction



Approach

- Include membrane and interface elements to model geogrid and soil-geogrid interaction, respectively.
- Geogrid membrane element (plane stress)
- Interface element linear elastic relation
 - Shear stiffness, k_s
 - Normal stiffness, k_n
 - Displacement components u, v, w .

$$\begin{Bmatrix} d\sigma_n \\ d\tau_x \\ d\tau_z \end{Bmatrix} = \begin{bmatrix} k_n & 0 & 0 \\ 0 & k_s & 0 \\ 0 & 0 & k_s \end{bmatrix} \begin{Bmatrix} dv \\ du \\ dw \end{Bmatrix}$$

Pavement distress models

- Rutting model
 - Progress of rutting with load repetition
 - ε_p : accumulated permanent strain
 - ε_r : resilient elastic strain
 - N : load cycle number
 - Material parameters
 - α : rate of increase in permanent deformation against the number of load applications
 - μ : permanent deformation
 - Difference in deflections of the top and bottom of the layer
- Failure criterion: 1-in. rutting

$$\varepsilon_p = \frac{\mu}{1 - \alpha} \cdot \varepsilon_r \cdot N^{1-\alpha}$$

Pavement distress models

- Fatigue cracking generated from tensile strains occurring at the bottom of the asphalt layers
- Fatigue model

- N_f : the number of load applications to failure

$$N_f = k_1 \varepsilon_t^{-k_2} E_{ACP}^{-k_3}$$

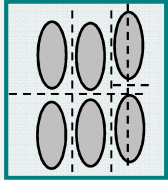

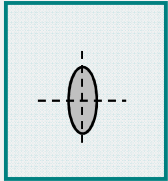

- $k_1 = 0.0796$, $k_2 = 3.291$, and $k_3 = 0.854$ are regression parameters based on a 20% failure area criterion and standard mix asphalt

Parametric studies

- Variation in layer thickness & geosynthetic location
- Utilization of C-17 and F-15 aircrafts
- Consideration of both biaxial and triaxial geogrids
- Rutting failure criteria of 1 inch
- Effectiveness of geosynthetic determined via traffic benefit ratio (TBR)
- Linear vs. non-linear
- Impact of base and subgrade modulus

In this study, the TBR values were determined based on the rut depth of 1 in. (25 mm) since failure in rutting occurred long before failure was reached in fatigue cracking for any of the pavements analyzed in this study.

Details of Aircraft Gears

Parameter	Aircraft type	
	C-17	F-15E Eagle
Maximum takeoff weight	585,000 lb (2600 kN)	81,000 lb (360 kN)
Landing gear designation and configuration	TRT - triple tandem tricycle  	S – Single wheel  
Landing gear load	269,217 lb (1200 kN)	70,470 lb (313.5 kN)
Strut spacing	93 in. (2.36 m)	-
Tire spacing	42 in. (1.07 m)	-
Dimensions	22.8 in. × 13.8 in. (580 mm × 350.5 mm)	13.4 in. × 8.1 in. (340 mm × 206 mm)
Contact area	314 in ² (202,580 mm ²)	108.5 in ² (69,700 mm ²)
Tire pressure	140 psi (965 kPa)	325 psi (2240 kPa)

Geogrids

- Geogrids considered for parametric studies

Type	Parameter	Properties	
		Machine Direction (MD)	Cross Machine Direction (XMD)
Biaxial	Minimum rib thickness	1.27 mm (0.05 in.)	1.27 mm (0.05 in.)
	Tensile strength @2% strain	6.0 kN/m (410 lb/ft)	9.0 kN/m (620 lb/ft)
	Aperture stability	650 N-mm/deg (5.7 lb-in./deg)	
Triaxial	Mid-rib depth	1.2 mm (0.05 in.)	1.2 mm (0.05 in.)
	Mid-rib width	1.1 mm (0.04 in.)	1.1 mm (0.04 in.)
	Tensile strength @0.5% strain	1.1 kN/m (77 lb/ft)	
	Aperture stability	300 N-mm/deg (2.6 lb-in./deg)	

Geogrids: Linear Elastic Properties

- Elastic modulus of the geogrid, E_g , is determined from the tensile stiffness, J_g , and the geogrid thickness, t , using
 - where J_g can be estimated from the tensile strength, T_{ε_a} , at a certain level of axial strain, ε_a , from
 - and the geogrid shear modulus, G (kPa), is related to the measured aperture stability modulus, ASM (N-mm/degree) of the geosynthetics by
- Geosynthetic tensile properties

$$E_g = \frac{J_g}{t}$$

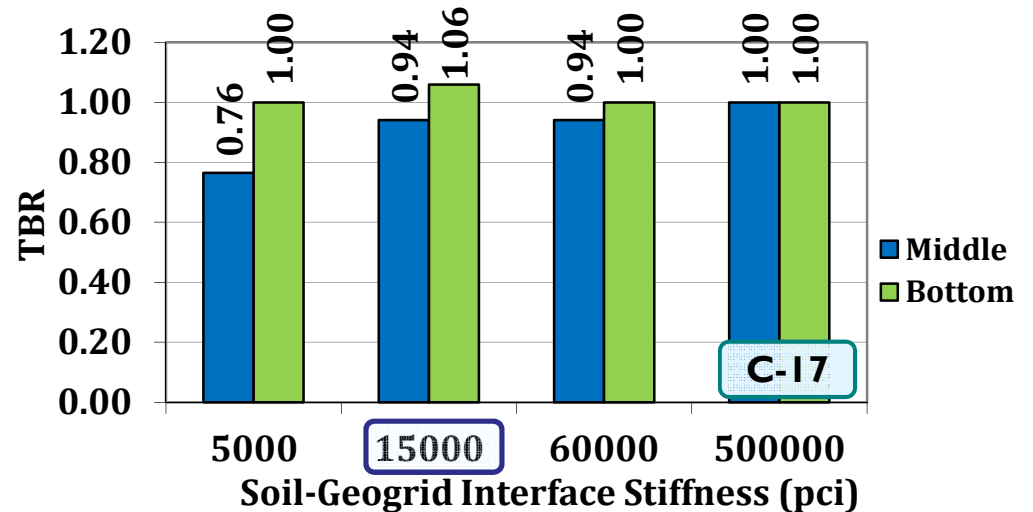
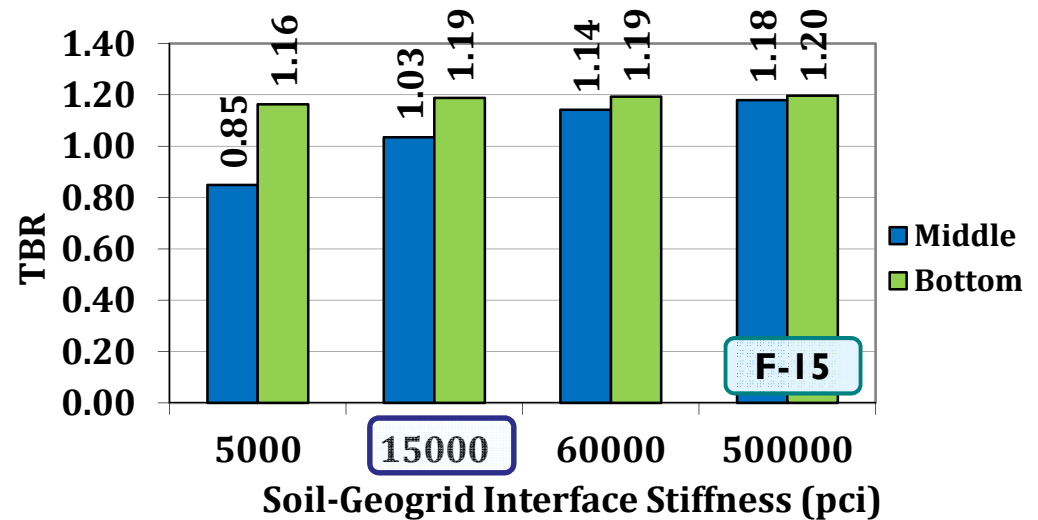
$$J_g = \frac{T_{\varepsilon_a}}{\varepsilon_a}$$

$$G = 7 ASM$$

Parameter	Geosynthetic	
	Biaxial	Triaxial
Modulus in machine direction, E_m	34 ksi (236 MPa)	26 ksi (177 MPa)
Modulus in cross machine direction, E_{xm}	52 ksi (356 MPa)	26 ksi (177 MPa)
Poisson's ratio in cross-machine – machine direction, ν_{xm-m}	0.25	0.25
Geogrid shear modulus in cross-machine – machine plane, G_{xm-m}	660 psi (4550 kPa)	305 psi (2100 kPa)

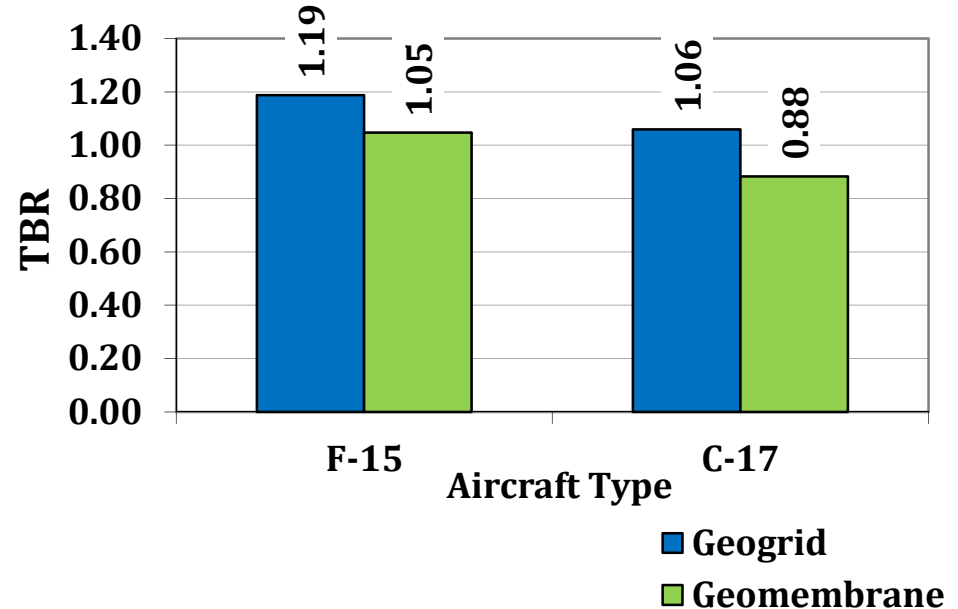
Soil-Geogrid Interface Shear Stiffness k_s

- Traffic Benefit Ratio (TBR)
 - 3-in. asphalt
 - 10-in. base
 - Varying k_s
- TBR is very sensitive to k_s when geogrid is placed at the mid-depth of the base
- Geogrids not effective in mitigating rutting for C-17



Geotextiles vs. Geogrids

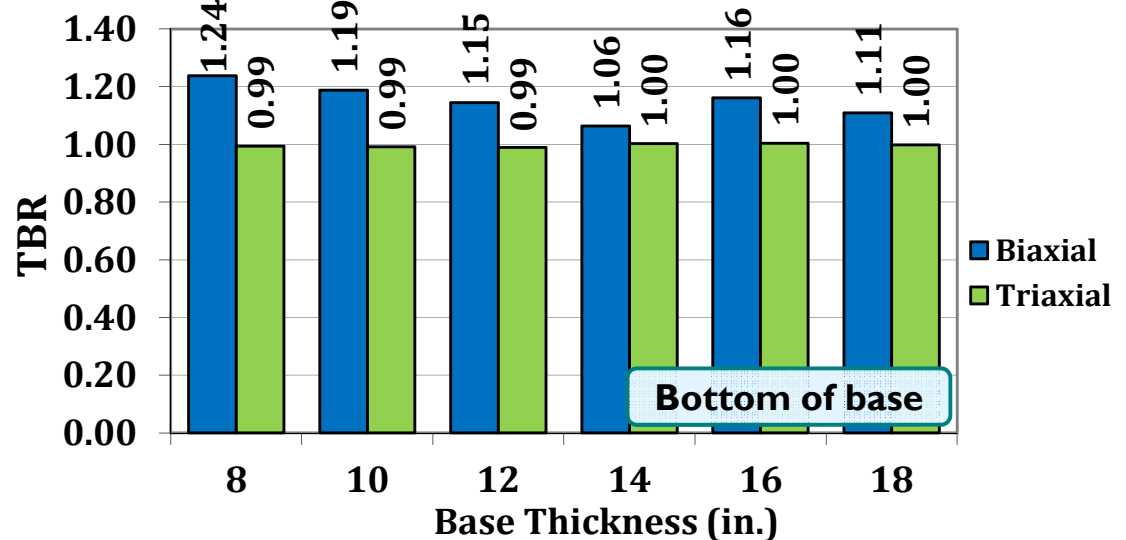
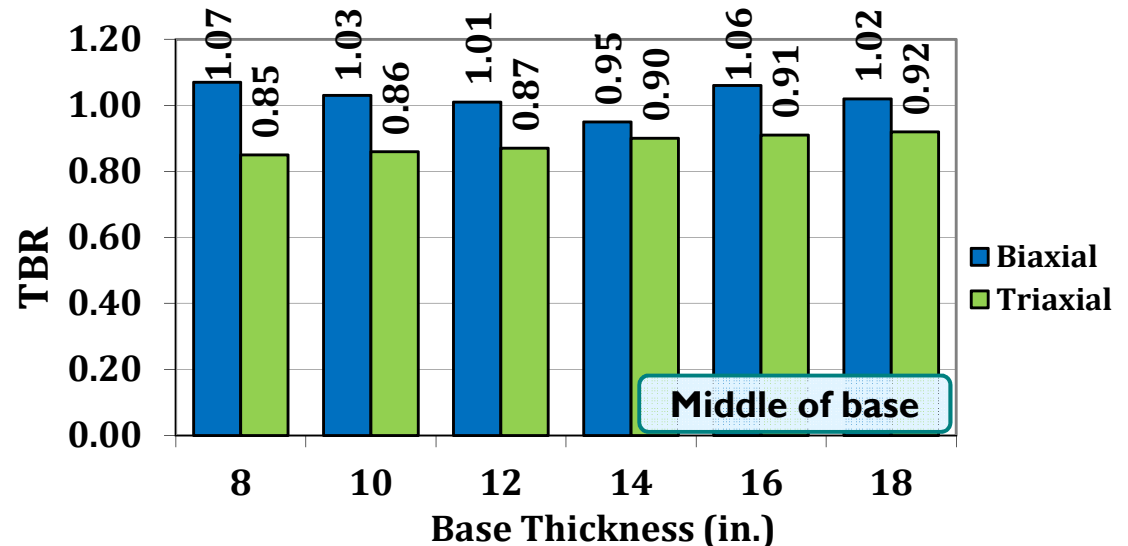
- Aperture size
 - Interlocking of base course aggregates
 - Geotextiles lack this feature
 - Prevent mixing of subgrade soil and granular base material
- Geogrids provide greater shear stiffness
- No benefit of geotextile materials



Type	Parameter	Properties	
		Machine Direction (MD)	Cross Machine Direction (XMD)
Geotextile: Amoco 2006	Tensile strength @2% strain	4.25 kN/m (290 lb/ft)	13.6 kN/m (930 lb/ft)
	Aperture stability	None	

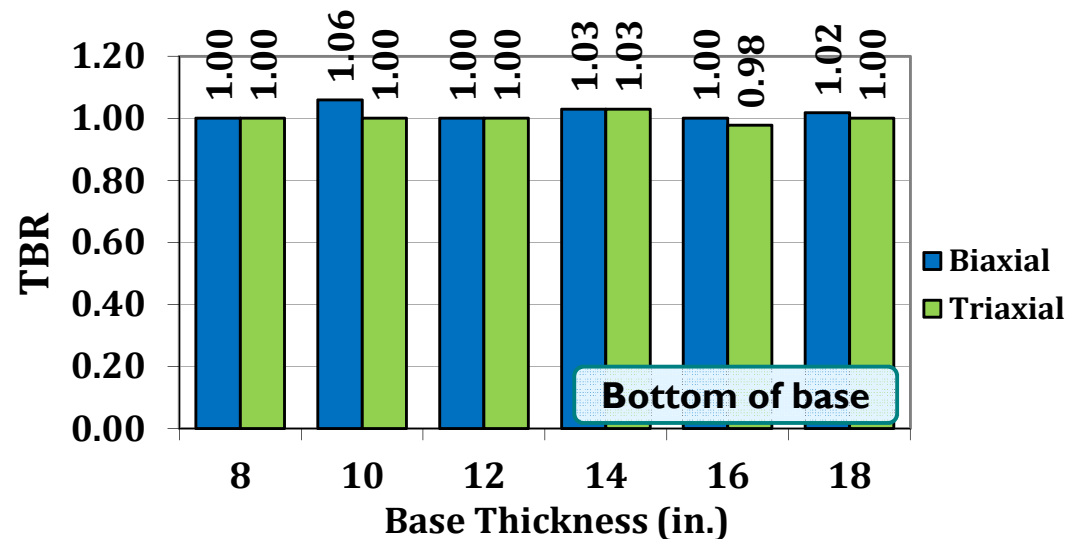
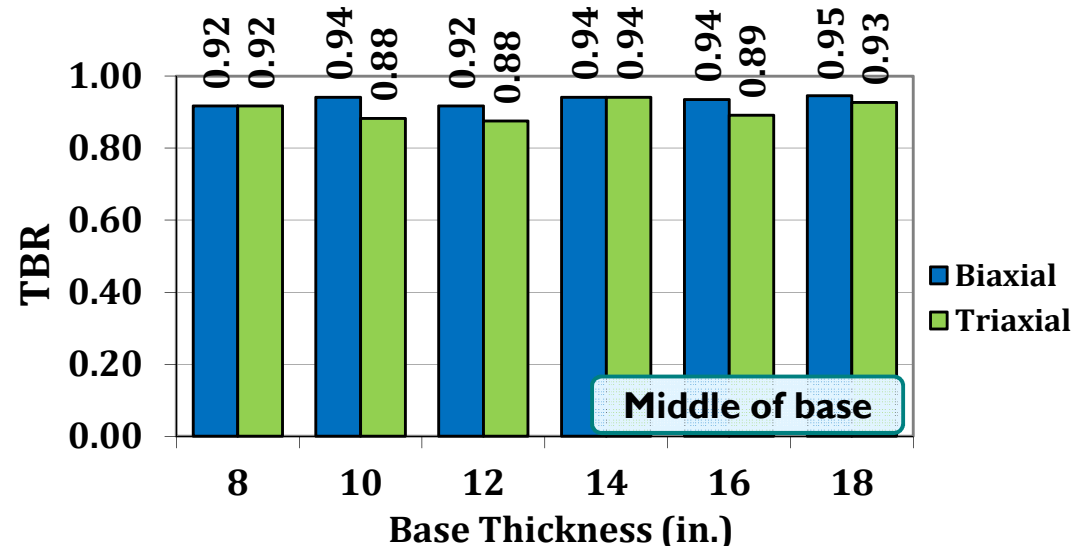
Biaxial vs. Triaxial (F-15 Aircraft)

- F-15 Aircraft
- Traffic Benefit Ratio (TBR)
 - 3-in. asphalt
 - Varying base thickness
- Weaker properties of triaxial geogrid



Biaxial vs. Triaxial (C-17 Aircraft)

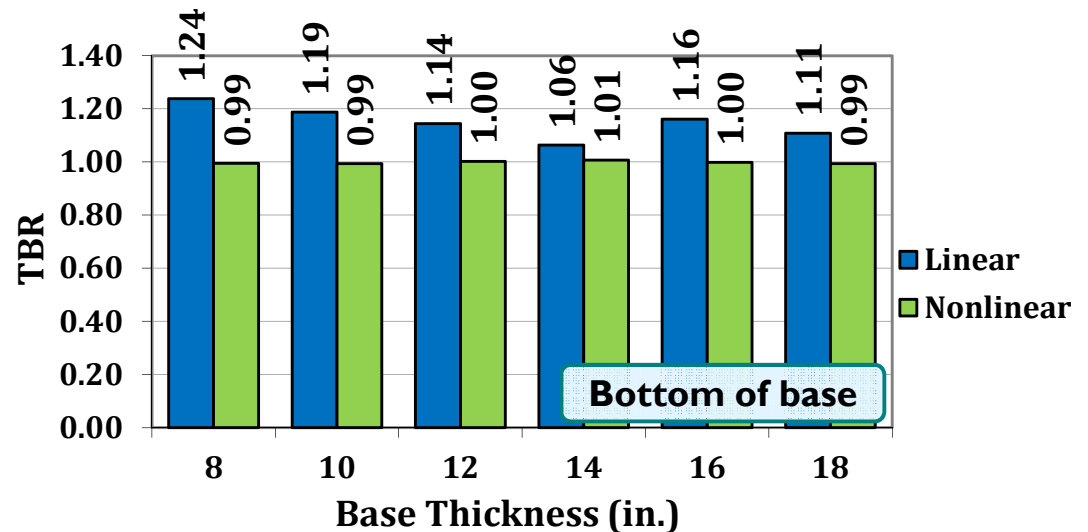
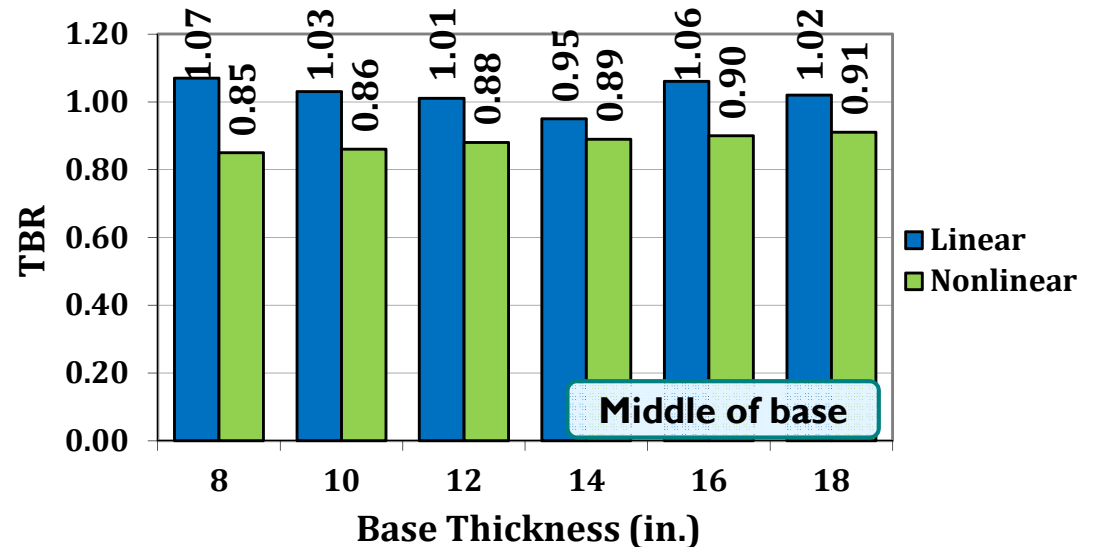
- C-17 Aircraft
- Traffic Benefit Ratio (TBR)
 - 3-in. asphalt
 - Varying base thickness
- No clear benefit when heavy loads with large contact areas are applied to the pavement.



Linear Elastic vs. Nonlinear Modeling of Base and Subgrade

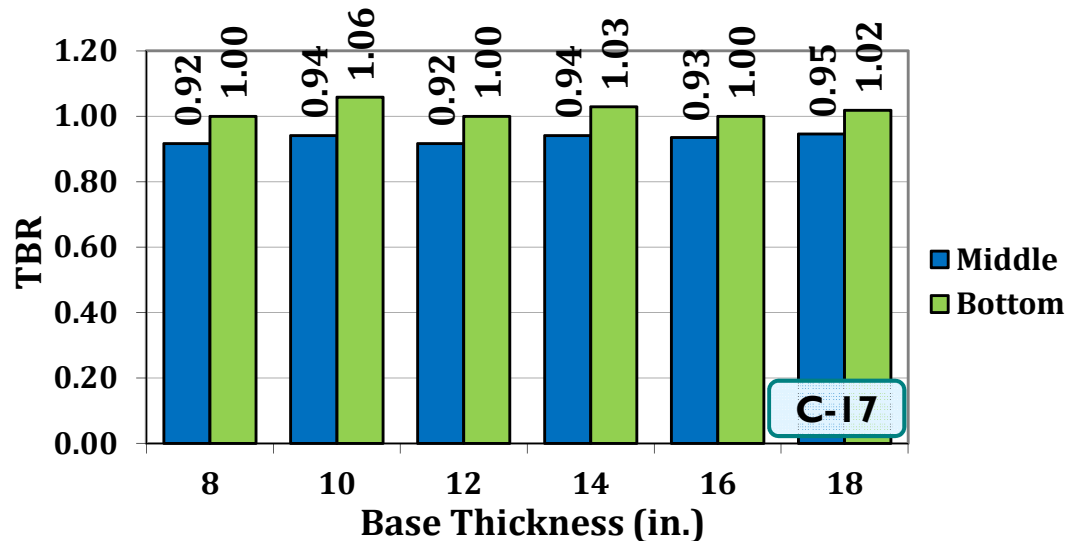
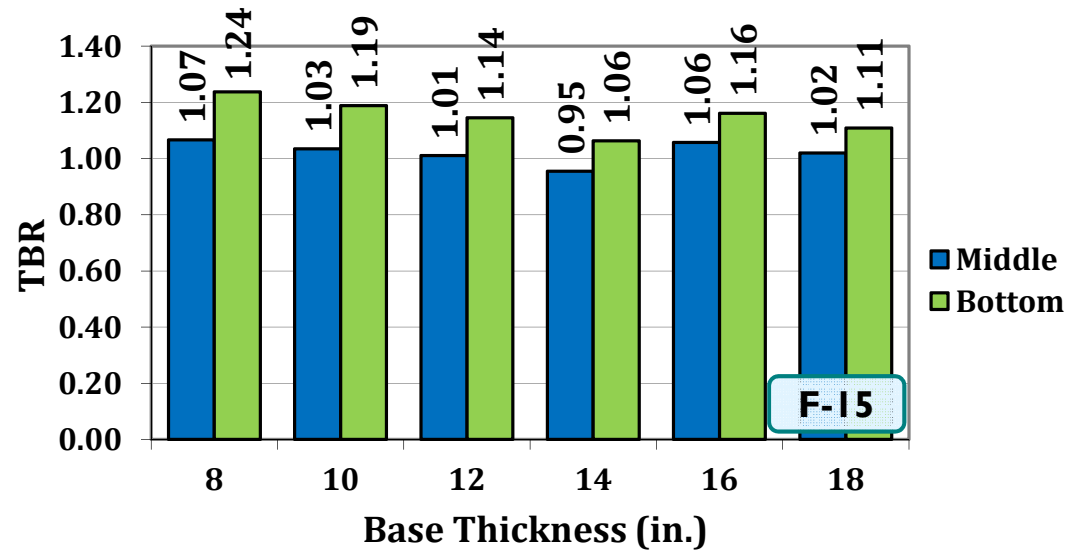
- Biaxial geogrid
- F-15 Aircraft
- Traffic Benefit Ratio (TBR)
 - 3-in. asphalt
 - Varying base thickness
- Similar pattern for C-17
- TBR decreased with respect to linear analyses

Layer	Nonlinear Parameters		
	k_1	k_2	k_3
Base	30,000 psi (207 MPa)	0.25	-0.25
Subgrade	5,000 psi (36 MPa)	0	-0.5

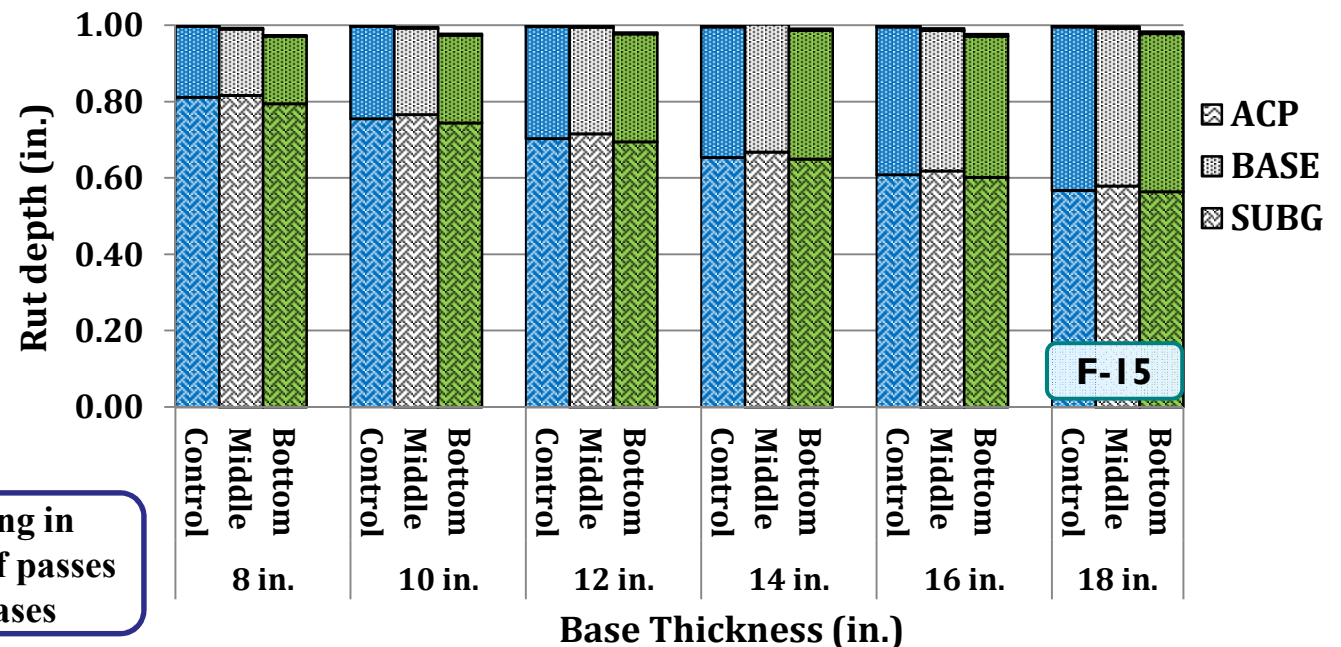
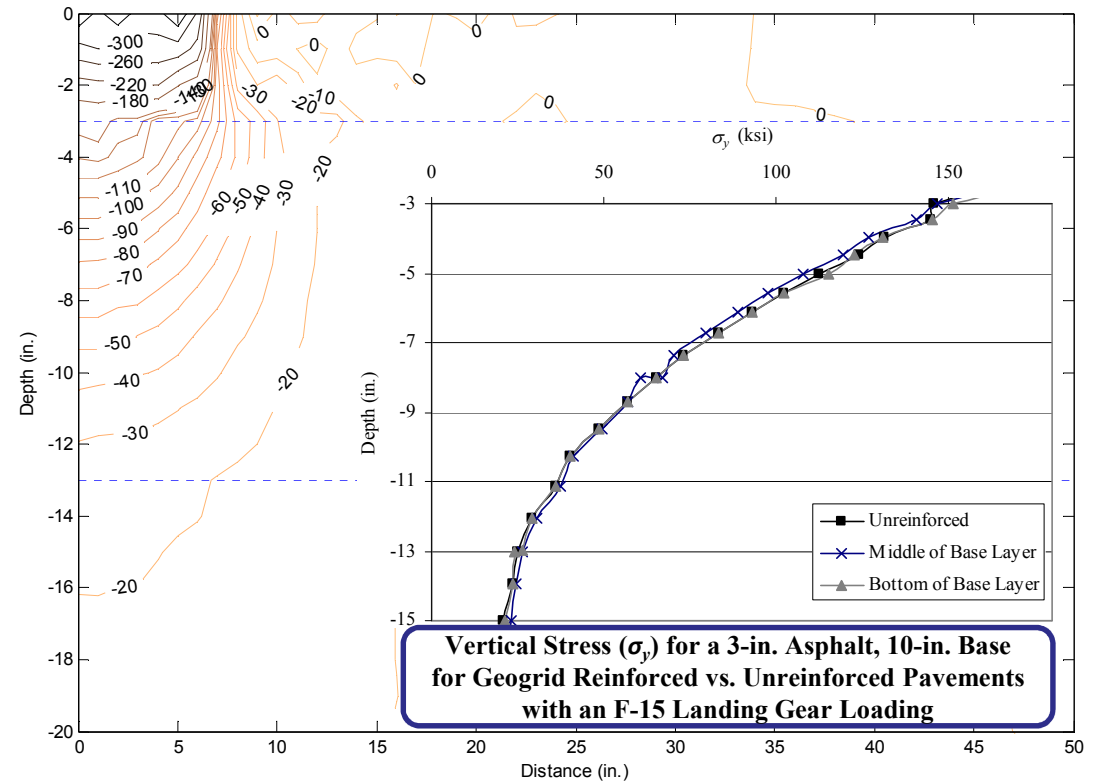


Impact of Base Thickness

- Traffic Benefit Ratio (TBR)
 - 3-in. asphalt
 - Varying base thickness
- Greater benefit observed when
 - Geogrid placed at bottom of base
 - F-15 aircraft
- Less benefit in thicker bases

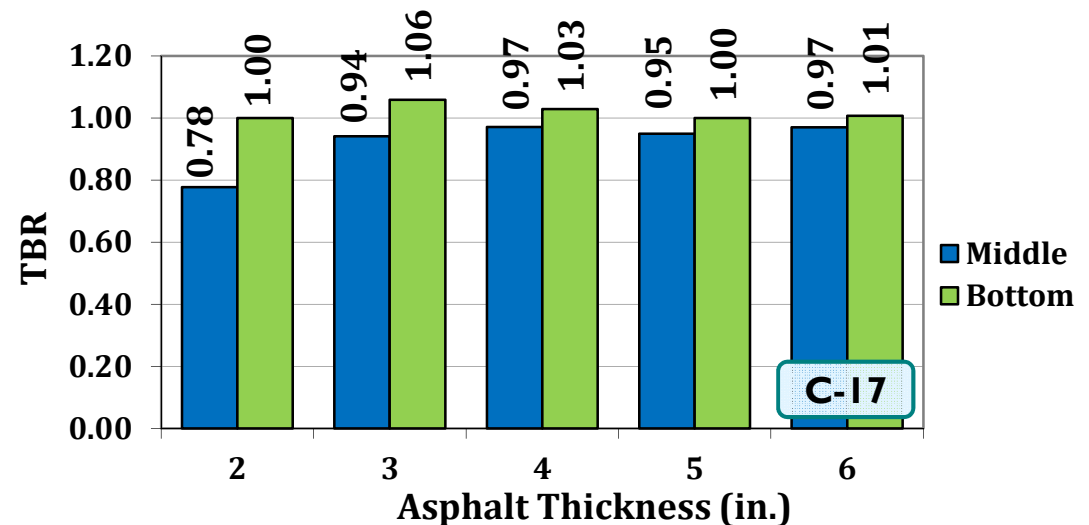
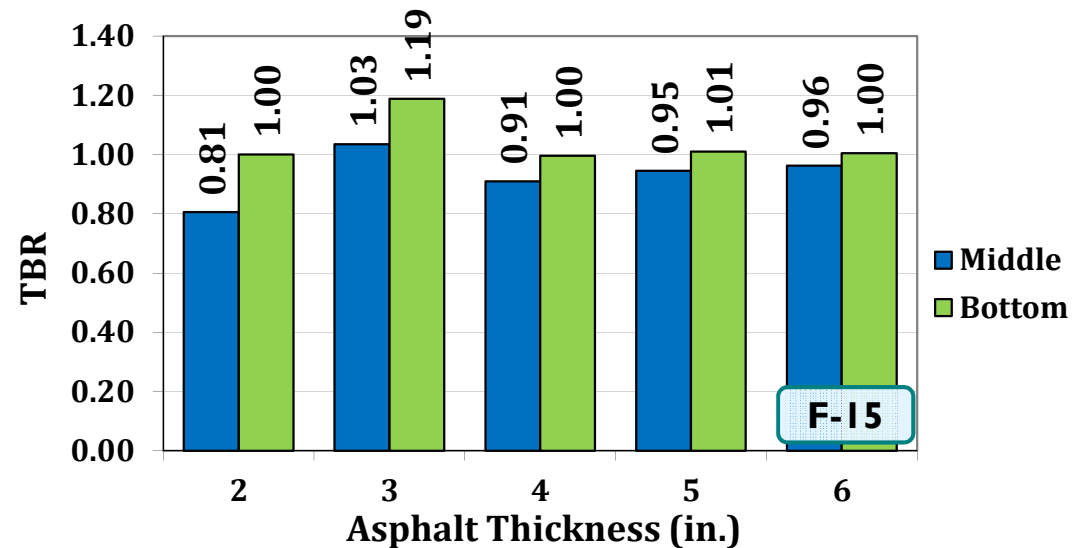


- Use of geogrid in the middle of the base transfers rutting from the base to the subgrade
- The proportion of rutting per layer remains the same when the geogrid is placed at the bottom of the base when compared to an unreinforced pavement.



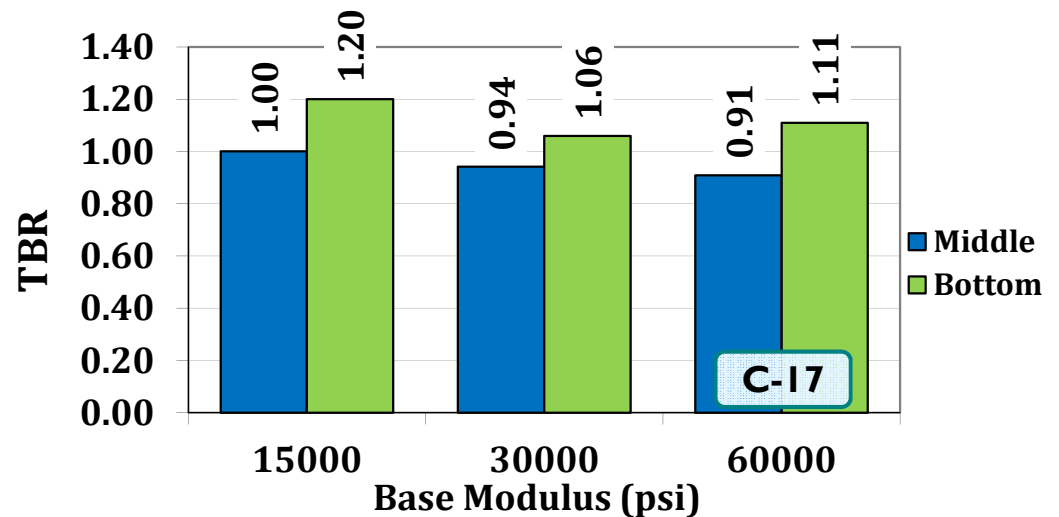
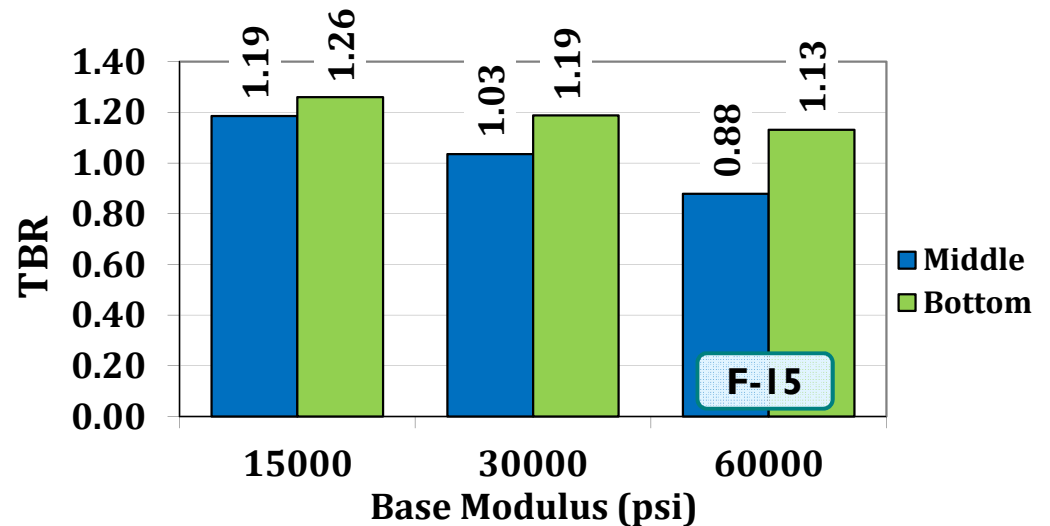
Impact of HMA Thickness

- Traffic Benefit Ratio (TBR)
 - Varying HMA thickness
 - 10-in. base
- Generally, no significant impact



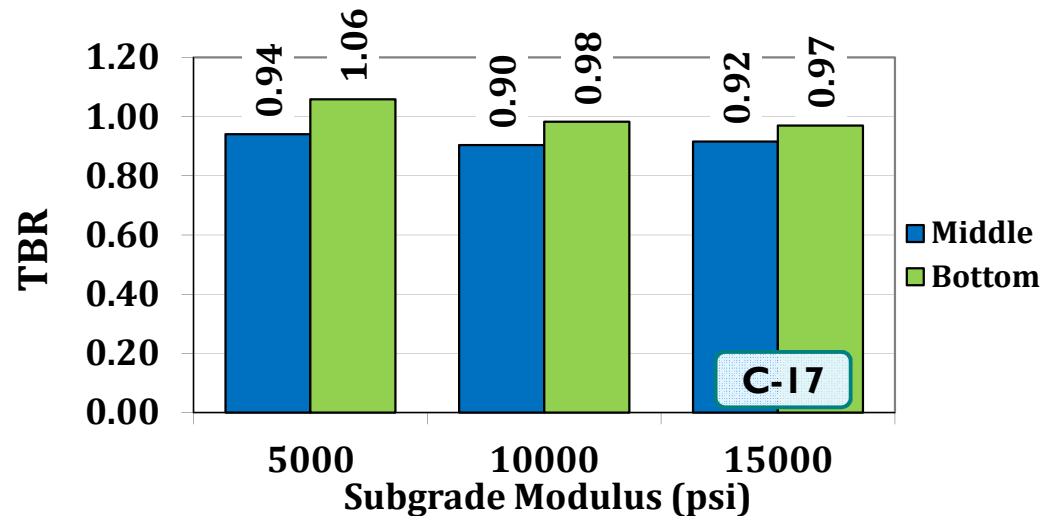
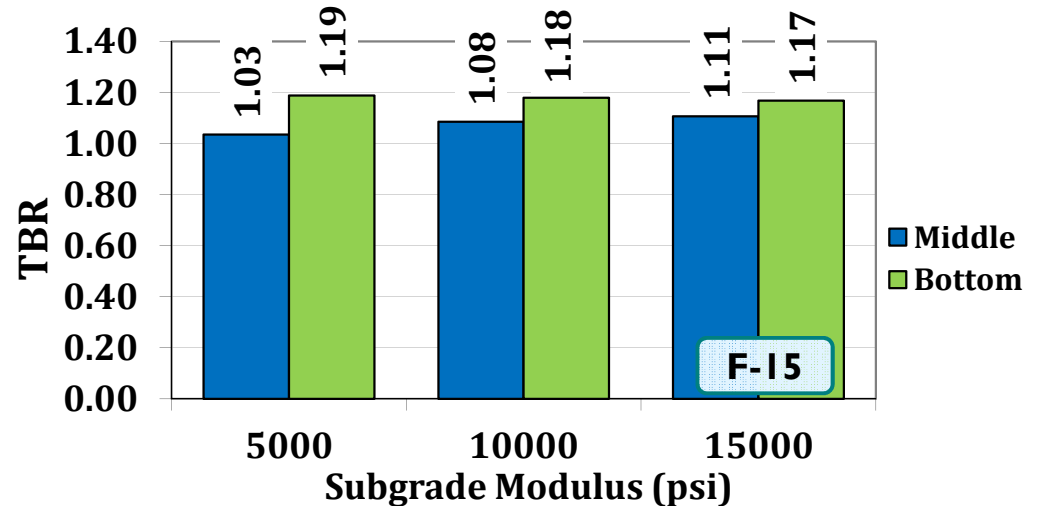
Impact of Base Modulus

- Traffic Benefit Ratio (TBR)
 - 3-in. asphalt
 - 10-in. base
- Effectiveness of geogrid diminishes as the base layer becomes stiffer
- Greater benefit observed when
 - Geogrid placed at bottom of base
 - F-15 aircraft



Impact of Subgrade Modulus

- Traffic Benefit Ratio (TBR)
 - 3-in. asphalt
 - 10-in. base
- Greater benefit observed when
 - F-15 aircraft
 - Geogrid placed at bottom of base for weaker bases
 - Geogrid placed in the middle of the base layer for stiffer bases



Summary and Recommendations

- TBR is moderately sensitive to HMA thickness
 - More significant for thinner HMA layers
- TBR is sensitive to thickness and modulus of the base mainly when reinforcement is below the base and an F-15 is considered
 - Benefit diminishes for thicker bases and is accentuated for less stiff bases.
- Effectiveness of geogrid reinforcement is significantly impacted by subgrade modulus
 - As the subgrade becomes stiffer, the percentage of rutting in the base layer increases.



Summary and Recommendations

- Benefit is more pronounced when an F-15 aircraft is considered moderate
- A significant component to the effectiveness of the geogrid is the type of the geogrid used as quantified by the soil/aggregate-geogrid interface shear stiffness
 - Particularly when the geogrid reinforcement is placed in the middle of the base.
 - Based on information available, the triaxial geogrid provides no added benefit when compared to the biaxial geogrid
 - This conclusion may change when more concrete information or standard test procedure become available about the interface shear stiffness.



Summary of Impact of Pavement Properties on TBR

		Aircraft Type				
		F-15		C-17		
		Location of Geogrid				
Property		Middle	Bottom	Middle	Bottom	
Geogrid						
HMA	Thickness					
Base	Thickness					
	Modulus					
Subgrade	Modulus					
Soil/Aggregate-Geogrid Interface	Shear Stiffness					
Triaxial						
Base	Thickness					
Geotextile/Geomembrane						
Base	Thickness					



Not significant: $0.95 \leq \text{TBR} \leq 1.05$

Moderately significant: $0.90 \leq \text{TBR} < 0.95$ and $1.05 < \text{TBR} \leq 1.10$

Significant: $\text{TBR} < 0.90$ and $\text{TBR} > 1.10$